TRIBOLOGY UPDATE: *ISSUE 38 – June 2020*

This is the latest issue of our **Tribology Update** newsletter. We find ourselves living in strange times! We very much hope that you and your families have remained safe.

We were in lock-down since the middle of March, with most staff working from home. Nobody has been laid-off; everybody has been retained, ready to contribute to our future.

With restrictions gradually being lifted in May, we started allowing up to two people into the workshop at a time, so production continued slowly. We are hopeful that we will soon be able to get output back up to more normal levels.

The one area where we can, at present, see no end in sight, is the restriction on international travel. Even after countries lift travel bans, there is currently no indication when it will again be possible to get insurance cover for our staff, travelling and working abroad.

WORK IN PROGRESS – DEVELOPMENT

TE 92 Plain Thrust Bearing Test Adapter

A paper by researchers at the University of Leoben reported on experiments performed on a TE 92 rotary tribometer, using a novel plain thrust bearing type test geometry:

Tribological performance of thin overlays for journal bearings

F Grun, I Godor, W Gartner

Tribology International Volume 44, Issue 11, October 2011, Pages 1271-1280

An interesting feature of their experiments was that they used a conventional parallel taper land/flat land thrust bearing arrangement, with six lands. In a flat land thrust bearing, where the surfaces are parallel, there is no mechanism for generating hydrodynamic pressure, so the contact will always run under boundary or, at best, mixed lubrication. The converging wedge, formed by a tapered land, will generate hydrodynamic lift, providing there is sufficient entrainment velocity.

At low speeds, there is low entrainment, so minimal hydrodynamic lift. This means that the load is carried more or less entirely on the flat land area, which is running under boundary lubrication. As the speed is increased, the entrainment velocity increases and the converging wedge starts to generate hydrodynamic lift, progressively separating the flat land surfaces and moving the contact from boundary to mixed and, eventually, hydrodynamic lubrication. Controlling the velocity thus provides an effective means of controlling the lubricant film thickness in the contact. There are a couple of practical issues with this arrangement. Firstly, it is obviously an expensive and difficult process manufacturing a small, six land, taper land/flat land bearing sample. Secondly, with a small mean friction diameter, the contact width is potentially too small to prevent significant radial leakage, from the contact.

To address these issues, we have been developing a new adapter that uses just three removable bearing pads, which can be either taper/flat, pure taper or pure flat profile. By mounting the pads centrally on a diameter, the contact width is maximised; this would not be the optimum choice if we were designing an actual thrust bearing, but is a good practical choice, for a test geometry.



The pad specimens can be manufactured as a single strip of material and finished either transversely or axially, then cut to the required length.

By electrically insulating each pad, independent electrical contact resistance measurements can be made, for each contact.

High Throughput Tribometers

At STLE 2018, Brendan Nation, John Curry, Michael Dugger and Greg Poulter, of Sandia National Laboratories, gave a presentation with the title:

"High Throughput Tribometry"

It included the question:

"Can we do 100 tests per day on the same piece of equipment?"

More recently, an industrial client commented:

"Capital cost is of importance as funding is tight and will not get better in the near future. You must bear in mind that for industry, testing time is seen in money terms: we need quick results, with dedicated units, which can easily be operated by an ordinary worker and not require 'scientists'."

We have, ourselves, been thinking about the requirement for high throughput friction and wear testing, and indeed, already have a number of multi-station rigs, which address the requirement. However, we have never really had time, until now, to address the matter in a concerted and coordinated fashion; we have taken the opportunity of the pandemic lock-down to do just that.

There is a further motivation behind designing a range of low cost, easy to operate, single function, high throughput machines and that is that we can substantially eliminate the requirement for installation, commissioning and training, which is usually necessary with more complicated, multi-function tribometers. The reason for this, of course, is that for the foreseeable future, visits to clients' facilities, are not possible.

General Concept

- Single function
- Multi-station
- Simple to Operate
- Control via PLC
- Data exported on USB stick

HTP 010 Two/Four Station Short Stroke Reciprocating

Evolution: TE 90 Two/Four Station Reciprocating Tribometer





Specification	Short Stroke Reciprocating	
Motion	Reciprocating	
Load	5 to 100	Ν
Stroke	5	mm
Frequency	3 to 30	Hz
Temperature	Ambient to 200	°C
Test Stations	2 or 4	
Manually Set Parameters		
Load	Yes - pneumatic	
Frequency	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Temperature	Yes - each sample	
Friction Force	Yes - each sample	
Contact Potential	Yes - each sample	

HTP 020 Three Station Thrust Washer

Evolution: TE 94 Three Station Rotary Tribometer







Specification	Thrust Washer	
Motion	Rotary	
Load	20 to 400	Ν
Diameter	ASTM D3702 Small/Large	mm
Speed	6 to 600	rpm
Temperature	Ambient to 150	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - pneumatic	
Rotational Speed	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Temperature	Yes - each sample	
Friction Force	Yes - each sample	

HTP 030 Three Station Four Ball Friction & Wear

Evolution: TE 94 Three Station Rotary Tribometer



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Specification	Four Ball Friction & Wear	
Motion	Rotary	
Load	20 to 400	Ν
Diameter	12.7	mm
Speed	50 to 1200	rpm
Temperature	Ambient to 150	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - pneumatic	

Rotational Speed	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Temperature	Yes - each sample	
Friction Force	Yes - each sample	

HTP 040 Six Station Cross Cylinder/Block on Ring

Evolution: Lathe Wear Generator





Specification	Cross Cylinder/Block on Ring	
Motion	Rotary	
Load	20 to 400	Ν
Diameter	20	mm
Speed	6 to 600	rpm
Temperature	Ambient	°C
Test Stations	6	
Manually Set Parameters		
Load	Yes - pneumatic	
Rotational Speed	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Friction Force	Sum total for all samples	

HTP 050 Three Station Sand - Wheel Abrasion - Dry & Wet

Evolution: TE 65 Sand/Wheel Abrasion Tester







	Sand - Wheel Abrasion - Dry &	
Specification	Wet	
Motion	Rotary	
Load	5 to 100	Ν
Diameter	80	mm
Speed	30 to 150	rpm
Temperature	Ambient	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - Pneumatic	
Rotational Speed	Yes	
Test Duration	Yes	
Data Logged Parameters	N/A	

HTP 060 Three Station Pin on Disc

Evolution: TE 79 Multi-Axis Tribology Machine







Specification	Pin on Disc	
Motion	Rotary	
Load	1 to 60	N
Diameter	75	mm
Speed	2 to 200	rpm
Temperature	Ambient to 200	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - dead-weight	
Rotational Speed	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Temperature	Yes - each sample	
Friction Force	Yes - each sample	

HTP 070 Three Station Block on Ring Friction

Evolution: TE 56 Multi Station Block on Ring Machine





Specification	Block on Ring Friction	
Motion	Rotary	
Load	5 to 150	Ν
Diameter	100	mm
Speed	10 to 380	rpm
Temperature	Ambient	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - Pneumatic	
Rotational Speed	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Friction Force	Yes - each sample	
Temperature	Yes - each sample	

HTP 080 Twelve Station Long Stroke Pin on Reciprocating Plate

Evolution: TE 87 Circular Translation Pin on Disc + TE 88 Friction & Wear Tester





Specification	Long Stroke Pin on Reciprocating Plate	
Motion	Reciprocating	
Load	5 to 100	Ν
Stroke	25	mm
Frequency	1 to 3	Hz
Temperature	Ambient to 150	°C
Test Stations	12	

Manually Set Parameters		
Load	Yes - pneumatic	
Frequency	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Load	Pressure Transducer	
Temperature	Yes	
Friction Force	Sum total for all samples	

HTP 090 Three Station Ball Cratering/Microscale Abrasion

Evolution: TE 66 Micro Scale Abrasion Tester







	Ball Cratering/Microscale	
Specification	Abrasion	
Motion	Rotary	
Load	0.1 to 5	Ν
Diameter	25	mm
Speed	30 to 150	rpm
Temperature	Ambient	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - dead-weight	
Rotational Speed	Yes	
Test Duration	Yes	
Data Logged Parameters	N/A	

HTP 100 Three Station High Temperature Pin on Disc

Evolution: TE 98 High Temperature Pin on Disc Machine







Specification	High Temperature Pin on Disc	
Motion	Rotary	
Load	1 to 60	Ν
Diameter	75	mm
Speed	2 to 200	rpm
Temperature	Ambient to 500	°C
Test Stations	3	
Manually Set Parameters		
Load	Yes - dead-weight	
Rotational Speed	Yes	
Temperature	Yes	
Test Duration	Yes	
Data Logged Parameters		
Temperature	Yes	
Friction Force	Yes - each sample	

For further information please e-mail: <u>high-throughput@phoenix-tribology.com</u>

WORK IN PROGRESS – PRODUCTION

High Pressure Hydrogen Reciprocating Tribometer





We are currently designing a reciprocating tribometer to work under pressurised hydrogen. This is, of course, somewhat more complicated than simply putting a conventional atmospheric tribometer in a pressure vessel. Firstly, the design has to be compliant with a number of EU directives including Pressure Systems Safety Regulations 2000 (PSSR), Dangerous Substances and Explosive Atmospheres Regulations 2002 (DSEAR) and ATmospheres EXplosible Directive 2014 (ATEX). Secondly, because of the time taken to purge the chamber of oxygen, then slowly pressurise with hydrogen, then allow the test specimens to absord hydrogen, it makes sense to fit as many test stations as possible, into the smallest enclosed volume as possible. A further complication is a requirement both to heat and to cool the test specimens.

Specification	
Number of Test Stations	Three
Test Configuration	Ball on flat
Gases	Hydrogen, Argon, CO2

Working Pressure	0.1 mbar to 120 bar
Stroke Range	0 to 20 mm Continuously Adjustable
Frequency	0 to 5 Hz
Load (dead-weight)	5 to 50 N
Temperature Range	-55°C to 150°C
Wear Range	0 to 100 microns

OTHER NEWS

On-line Tutorials

We have now produced YouTube videos, based on material delivered during the Cambridge Tribology Course, plus other events at STLE, Wear of Materials etc. These can be viewed either via our web site or direct on YouTube at:

Tribology Testing

Engine Tribology

Lubricated Friction

Lubricated Wear

If you would like copies of the PowerPoint slides, please e-mail <u>tutorial@phoenix-</u> <u>tribology.com</u>, with the subject the title you wish to receive.

IET TV Video

The following was recorded at a Tribology UK meeting in 2015. If you have time to waste, you may find it entertaining!

Why Become a Tribologist? - A personal view, with reference to those who have influenced me

George Plint and David Harris

Phoenix Tribology Ltd